

Europäisches Patentamt
Europ an Pat nt Office
Office uropéen des brevets



(11) **EP 1 094 574 A1**

(12)

EUROPEAN PATENT APPLICATION

(43) Date of publication:
25.04.2001 Bulletin 2001/17

(51) Int Cl.7: **H01S 5/026, H01S 5/12,**
H01S 5/0625

(21) Application number: 99870214.6

(22) Date of filing: 18.10.1999

(84) Designated Contracting States:
AT BE CH CY DE DK ES FI FR GB GR IE IT LI LU
MC NL PT SE
Designated Extension States:
AL LT LV MK RO SI

(71) Applicants:
• **INTERUNIVERSITAIR MICRO-ELEKTRONICA**
CENTRUM VZW
3001 Heverlee (BE)
• **Universiteit Gent**
9000 Gent (BE)

(72) Inventors:
• **Sarlet, Gert**
8000 Brugge (BE)
• **Buus, Jens**
Gayton Northants NN7 3EZ (GB)
• **Baets, Roel**
9800 Deinze (BE)

(74) Representative: **Van Malderen, Joelle et al**
Office Van Malderen,
Place Reine Fabiola 6/1
1083 Bruxelles (BE)

(54) **Widely wavelength tunable integrated semiconductor device and method for widely wavelength tuning semiconductor devices**

(57) Alternative laser structures, which have potentially the same tuning performance as (S)SG-DBR and GCSR lasers, and a fabrication process which is similar

to that of the (S)SG-DBR laser, are presented. The advantage of these structures is that the output power does not pass through a long passive region.

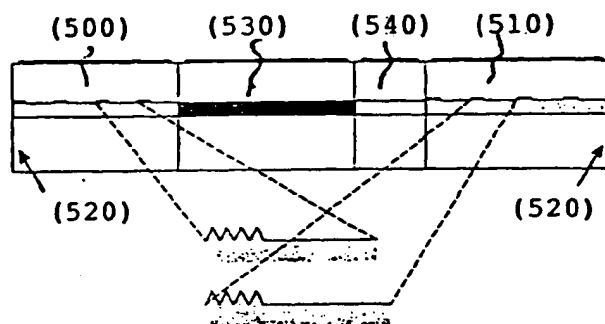


FIG. 1

Description

Field of the Invention

[0001] The invention relates to multi-section integrated semiconducting devices or lasers, comprising resonator sections, being either distributed reflection or transmission sections. The invention also relates to methods for widely wavelength tuning semiconductor devices or lasers.

Background of the Invention

[0002] Tuning of a conventional Distributed Bragg Reflector (DBR) semiconductor laser is limited by the fact that the relative tuning range is restricted to the relative change in the refractive index of the tuning region. This means that the tuning range, under normal operating conditions, cannot exceed 10 nm. This is substantially less than the potential bandwidth, restricted by the width of the gain curve, which is about 100 nm. Such conventional DBR lasers can functionally be characterized as comprising a first part being a two-sided active section, for creating radiation, for instance a light beam, by spontaneous emission over a bandwidth around one center frequency. Said first part also guides said radiation or light beam. Such conventional DBR lasers further have two reflectors. Said reflectors are bounding said two-sided active section, thus one at each side.

[0003] Over the past years several advanced laser structures have been proposed with an extended tuning range. Examples are the Y-laser [M. Kuznetsov, P. Verlangieri, A.G. Dentai, C.H. Joyner, and C.A. Burrus, "Design of widely tunable semiconductor three-branch lasers," J. Lightwave Technol., vol. 12, no. 12, pp. 2100-2106, 1994], the co-directionally coupled twin-guide laser [M.-C. Amann, and S. Illek, "Tunable laser diodes utilizing transverse tuning scheme," J. Lightwave Technol., vol. 11, no. 7, pp. 1168-1182, 1993], the Sampled Grating (SG) DBR laser [V. Jayaraman, Z.M. Chuang, and L.A. Coldren, "Theory, design and performance of extended tuning range semiconductor lasers with sampled gratings," IEEE J. Quantum Electron., vol. 29, no. 6, pp. 1824-1834, 1993], the Super Structure Grating (SSG) DBR laser [H. Ishii, H. Tanobe, F. Kano, Y. Tohmori, Y. Kondo, and Y. Yoshikuni, "Quasi-continuous wavelength tuning in super-structure-grating (SSG) DBR lasers," IEEE J. Quantum Electron., vol. 32, no. 3, pp. 433-440, 1996] and the Grating assisted Coupler with rear Sampled Reflector (GCSR) laser [M. Öberg, S. Nilsson, K. Streubel, L. Backbom, and T. Klinga, "74 nm wavelength tuning range of an InGaAsP/InP vertical grating assisted codirectional coupler laser with rear sampled grating reflector," IEEE Photon. Technol. Lett., vol. 5, no. 7, pp. 735-738, 1993]. In the first two types of devices, a trade-off had to be made between the tuning range and the spectral purity (broad tuning range vs. high Side Mode Suppression Ratio (SMSR)).

Therefore recently most research attention has gone to the (S)SG-DBR and GCSR lasers.

[0004] A sampled grating DBR laser, comprises of two sampled gratings exhibiting a comb-shaped reflectance spectrum, with slightly different peak spacing due to the different sampling periods. As an alternative, other grating shapes can be used: these are normally referred to as "super structure gratings" (SSG). Lasers of this type have been fabricated with tuning ranges up to about 100 nm. The operation of the device is such that through current injection in the two DBR sections, a peak of the front and rear reflectance comb are aligned at the desired wavelength. The phase section is used to align a longitudinal cavity mode with the peaks of the two reflectors. The disadvantage of the (S)SG-DBR approach is that light coupled out of the laser has to pass a long passive or inactive section, leading to loss. Also, the losses in the two reflector sections increase with the amount of current injected into those sections, leading to a tuning current dependent output power.

[0005] The SG-DBR laser and the SSG-DBR laser are functionally characterized as comprising a two-sided active region for light creation and two reflectors one at each side of the active region, said reflectors having a reflection characteristic with a plurality of reflection peaks. Said characteristic has spaced reflection maxima points providing a maximum reflection of an associated wavelength. Such a characteristic can be obtained via sampled gratings, which exhibit a comb-shaped reflection spectrum or via the so-called supergratings. Said gratings or supergratings can also be characterized as distributed reflectors.

[0006] Sampled gratings can be described as structures in a waveguide system, having a periodically broken short-period structure including short period stripped regions alternating with non-stripped regions. The supergratings can be described as structures in a waveguide system having a diffractive grating having a plurality of repeating unit regions, each having a constant length, thus forming a modulation period, and at least one parameter that determines the optical reflectivity of said diffractive grating varying depending on its position in each of said repeating unit regions along a direction of optical transmission in said laser, said diffractive grating extending by at least two modulation periods. Reference is made to US patent US5,325,392 related to distributed reflector and wavelength tunable semiconductor lasers, hereby incorporated by reference.

[0007] The SG-DBR laser and the SSG-DBR laser are exploiting constructive interference of the periodic characteristics of reflectors, located at different sides of the active section, with different periodicity, to obtain a wide tunability. The alignment of the reflector peaks can be described by stating that the spacing of said reflective maxima points of the reflectors are different or are essentially not equal and only one said reflective maxima of each of said reflectors is in correspondence with a

wavelength of said created lightbeam. Reference is made to patent US-A-4,896,325, related to multi-section tunable lasers with differing multi-element mirrors, hereby incorporated by reference.

[0008] As the construction of said reflectors leads to long inactive sections, this results in lasing output power losses.

[0009] Other lasers, which use a co-directional coupler, readily have a very wide tuning range, but there is insufficient suppression of neighbouring longitudinal modes. The combination of a widely tuneable but poorly selective co-directional coupler with a single (S)SG reflector will give both wide tuning and a good side mode suppression. Furthermore, the optical output signal does not pass through a passive region. Again tuning of 100 nm has been achieved. Unfortunately, such a structure is rather complicated to manufacture, requiring at least 5 growth steps. Reference is made to patent US-A-5,621,828 related to integrated tunable filters, hereby incorporated by reference.

Aim of the invention

[0010] The aim of the present invention is to disclose laser structures which are easy to manufacture and which are widely tuneable and have low lasing output power losses.

Summary of the invention

[0011] In the present invention alternative laser structures, apparatus or devices, which have potentially the same tuning performance as (S)SG-DBR and GCSR lasers and which output power does not pass through a long passive region, are presented.

[0012] An integrated/semiconductor tunable laser comprising a substrate made of a semiconducting material, a two-sided active section on said substrate, and a plurality of sections on said substrate, is disclosed. Said laser can be denoted as a multi-section integrated semiconductor laser. Said active section is radiation generating, for instance, but not limited to the range of optical radiation. All said sections are connected to one side of said active section. Note that this does not mean that they are directly coupled to said active section. In case of optical radiation said connection can be denoted as an optical connection. At least two of said sections include a waveguide system. Each of said sections defines a resonator. Said resonator can be either a transmission filter or a reflector.

[0013] The resonators used in the present invention have resonance characteristics with a plurality of resonance peaks. Alternatively it can be said that said resonators have spaced resonance maxima points providing a maximum resonance of an associated wavelength. The transmission filters used in the present invention have a transmission characteristic with a plurality of transmission peaks. Alternatively it can be said that said

transmission filters have spaced transmission maxima points providing a maximum transmission of an associated wavelength. The reflectors used in the present invention have a reflection characteristic with a plurality of reflection peaks. Alternatively it can be said that said reflectors have spaced reflective maxima points providing a maximum reflection of an associated wavelength.

[0014] The spacing of said resonator maxima points corresponding to the transmission or reflective maxima points of at least two of said sections are selected to be essentially not equal or different. Said laser is therefore denoted as an integrated semiconductor laser with different reflection or transmission sections. The transmission and reflection characteristic of said transmission filters and reflectors are positioned relative to each other such that at least one said transmission or reflective maxima of each of said two sections being overlapping each other. This means that said sections have at least one transmission or reflective maxima for a same first frequency. Due to the different spacings of said transmission or reflective maxima points a small shift of one of said transmission or reflective characteristics can result in overlapping of at least one other transmission or reflective maxima of each of said two sections. Said sections have then at least one second frequency in common, which can be largely different from said first frequency. Said shift can be due to current injections in said transmission or reflective sections. It can be said that said laser comprises means for injecting current into some of said plurality of sections, resulting in said transmission or reflection characteristic being shifted in wavelength. Said overlapping maxima points define a plurality of lasing wavelengths. Due to the small shifting of at least one resonator characteristic, said device jumps from a first set of lasing wavelengths to another set of lasing wavelengths.

[0015] It can be said that said active section creates a radiation or a lightbeam by emission and that the device emits an emitted laser beam with the wavelength of said emitted lightbeam being in correspondence with said overlapping maxima of said transmission filters or reflectors. Said active section is thus creating radiation or a light beam by spontaneous emission over a bandwidth around a center frequency and guides said radiation or light beam and has (optical) amplification actions. Said emitted radiation or lightbeam does not pass through said plurality of sections. The combination of said plurality of sections, having a combined reflection action, and said (optical) amplification action of said active section causes lasing at said set of lasing wavelengths. Due to the fact that small shifting of resonator characteristics results in large difference in the set of lasing wavelengths, an optical laser having a wide tunability, is obtained. Said laser is therefore denoted widely wavelength tunable integrated semiconductor laser.

[0016] In an embodiment of the invention only one of said resonator maxima points is overlapping. It can then be said that said active section creates a radiation or a

lightbeam by emission and the device emits an emitted laser beam with the wavelength of said emitted lightbeam being in correspondence with said overlapping maxima of said transmission filters or reflectors. The combination of said plurality of sections, having a combined reflection action with a single reflection wavelength, and said (optical) amplification action of said active section causes lasing at said single reflection wavelength, defined by said overlapping resonator maxima points.

[0017] In an embodiment of the invention at least one of said plurality of sections is inactive. This means that such inactive section is not creating a lightbeam by emission.

[0018] In an embodiment of the invention at least one of said plurality of sections is active. This means that such active section also creates a lightbeam by emission.

[0019] In an embodiment of the invention at least one of said waveguide systems has a periodically broken short-period structure including short period stripped regions alternating with non-stripped regions. Such waveguide systems are also denoted distributed, hence said laser is denoted a semiconductor laser with distributed reflection or transmission sections. In the invention two such waveguides can be found on the same side of the active region.

[0020] In an embodiment of the invention at least one of said waveguide systems has a diffractive grating having a plurality of repeating unit regions each having a constant length, thus forming a modulation period, and at least one parameter that determines the optical reflectivity or transmission of said diffractive grating varying depending on its position in each of said repeating unit regions along a direction of optical transmission in said laser, said diffractive grating extending by at least two modulation periods.

[0021] In an embodiment of the invention at least one of said waveguide systems is a ring resonator.

[0022] In an embodiment of the invention the laser comprises further of a plurality of power splitters, being exploited for optically connecting part of said plurality of sections and connecting part of said plurality of sections with said active section.

[0023] In an embodiment of the invention said laser is a serial concatenation of said active section and a plurality of said sections.

[0024] In an embodiment of the invention said laser is a connection of said active section to one single port side of a power splitter and a parallel connection of a plurality of sections to the other multi port side of said power splitter.

[0025] In an embodiment of the invention said laser comprises phase sections, being exploiting for adjusting the round trip cavity phase and thus a lasing mode wavelength of the laser.

Brief description of the invention

[0026] Fig. 1 is a longitudinal cross-section of an SG-DBR laser. As opposed to a conventional DBR laser, the reflectors are formed by two periodically modulated (sampled) gratings with different sampling periods.

[0027] Fig. 2 is a schematic diagram of a GCSR laser structure.

[0028] Fig. 3 is a top view (schematic) of the proposed "Y-SSG" laser.

[0029] Fig. 4 is a schematic view of a ring resonator (S)SG laser.

[0030] Fig. 5 is a transmission characteristic of a ring resonator.

[0031] Fig. 6 is a principle scheme of the laser according to the invention, comprising an active element and a plurality of sections, being either transmission filters or reflectors.

[0032] Fig. 7 is a principle scheme of prior-art lasers, comprising an active element and reflectors, said active element being bounded by said reflectors.

[0033] Fig. 8 is a principle scheme of the second embodiment of the invention, comprising an active element and a plurality of sections, being parallel.

[0034] Fig. 9 is a principle scheme of the fourth embodiment of the invention, comprising an active element and a serial concatenation of transmission filters ended by a reflector.

Detailed description of the invention

[0035] In the further description several embodiments of the invention are presented. It must be clear that the scope of the invention is described by the claims.

[0036] The present invention discloses alternative laser structures, which are potentially the same tuning performance as (S)SG-DBR and GCSR lasers and which the output power does not pass through a long passive region. In said devices there are passive or inactive regions on one side of the active region only.

[0037] A principle scheme of prior-art conventional Distributed Bragg Reflector (DBR) semiconductor laser is shown in Figure 7. A schematic description of such a laser is shown in Figure 1, showing a front (500) reflector, a rear reflector (510), an AR (anti-reflective coating), an active section (530) and a phase section (540). Tuning of said laser is limited by the fact that the relative tuning range (360) is restricted to the relative change in the refractive index of the tuning region. This means that the tuning range, under normal operating conditions, cannot exceed 10 nm. This is substantially less than the potential bandwidth, restricted by the width of the gain curve (350), which is about 100 nm. Such conventional DBR lasers can functionally be characterized as comprising a first part being a two-sided active section (300), for creating a light beam (310) by spontaneous emission over a bandwidth around some center frequency (370), as observed in said lasers characteristic (340). Said first

part also guides said light beam. Such conventional DBR lasers further have two reflectors (330)(320). Said reflectors are bounding said two-sided active section (300), thus one at each side.

[0038] A classical laser structure comprises (i) a two-sided active section/region, creating a light beam by spontaneous emission over a bandwidth around some center frequency and guiding said light beam, said active section performing optical amplification actions and (ii) two (inactive or passive) sections/regions, acting as reflectors. Said active section is bounded by said two reflectors.

[0039] Besides (inactive or passive) reflecting sections/regions, also sections with a transmission characteristic exist.

[0040] The invention can be characterized as comprising a two-sided active section/region (just as a classical laser) and a plurality of sections/regions. Said plurality of sections/regions defines a network of sections/regions. Said network of sections/regions is connected to one side of the active region. Said network comprises at least two resonator regions/sections. Said resonator regions/section can be either reflectors and regions/sections with a transmission characteristic. The principle scheme of the laser according to the invention, comprising an active element (30) and a plurality of sections (50) (90) (100) (110), being resonators, thus being either transmission filters or reflectors, is shown in Figure 6.

[0041] The invention can be characterized as a device comprising (i) a substrate made of a semiconducting material, (ii) a two-sided active section on said substrate, said active section generating radiation by spontaneous emission over a bandwidth around some center frequency and guiding said radiation, said active section having amplification actions, and (iii) a plurality of sections on said substrate, all said sections being connected to one side of said active section, at least two of said sections including a waveguide system, defining either a transmission filter or a reflector. The device can further be comprising a plurality of power splitters, being exploited for interconnecting part of said inactive sections and connecting part of said sections with said active section. Said sections can be either active or inactive.

[0042] When said device creates a light beam, said connection of said network with said active section is an optical connection. Said connections of said sections are then also optical. Said device can then be denoted as a tunable integrated/semiconductor optical laser. Said amplification is then denoted to be an optical amplification. Said active section then also guides said light beam.

[0043] In the invention particular reflectors and sections with transmission characteristics are exploited. Said reflectors and sections with transmission characteristics are commonly denoted as resonators. Said reflection and transmission sections are functionally characterized as having a reflection or transmission characteristic with a plurality of reflection or transmission

peaks, commonly denoted as resonance peaks. Said reflection or transmission characteristic has spaced reflection or transmission maxima points providing a maximum reflection or transmission of an associated wavelength. The resonator characteristic thus has a plurality of spectral response peaks, preferably narrow spectral response peaks. Said resonator characteristic can be either regular, meaning that its resonance frequencies are all spaced apart by a same value, being the periodicity, or irregular, meaning that there is no fixed spacing between its resonance frequencies. Irregularity can be a random pattern of resonance frequencies or some structured pattern.

[0044] Such a characteristic can be obtained via sampled gratings, which exhibit a comb-shaped reflection or transmission spectrum or via the so-called supergratings. Said gratings or supergratings can also be characterized as distributed reflectors or transmission sections.

[0045] Sampled gratings can be described as structures in a waveguide system, having a periodically broken short-period structure including short period stripped regions alternating with non-stripped regions. The supergratings can be described as structures in a waveguide system having a diffractive grating having a plurality of repeating unit regions each having a constant length, thus forming a modulation period, and at least one parameter that determines the optical reflectivity or transmission of said diffractive grating varying depending on its position in each of said repeating unit regions along a direction of optical transmission in said laser, said diffractive grating extending by at least two modulation periods.

[0046] In the invention alternative sections with transmission characteristics based on ring resonators are exploited. Such a ring resonator has a comb-shaped transmission characteristic (Figure 5). The operation of a ring resonator is similar to that of a classic Fabry-Perot resonator, which can easily be understood if one thinks of the cross-coupling of the two couplers in the ring as being the transmission mirrors in the FP-resonator.

[0047] In the prior art constructive interference of the periodic characteristics of reflectors, located at different sides of the active section, with different periodicity is exploited to obtain a wide tunability. As the construction of said reflectors leads to long inactive sections, this results in lasing output power losses.

[0048] In the invention constructive interference of the periodic characteristics of sections, being either reflective or transmissive, and with different periodicity and located at the same side of the active section is exploited. This approach results in wide tunability of said laser. Even when said reflectors are by construction long inactive sections, this is not harmful for the lasing output power, as these are only located at a single side of the active section. The invention results in a low loss window at any time.

[0049] Thus the invention can be further character-

ized by stating that the spacing of at least two transmission or reflective maxima points of the respective (inactive or even active) sections being essentially not equal or different, and at least one said transmission or reflective maxima of each of said (inactive or even active) sections being in correspondence with a wavelength of said created lightbeam. This correspondence is obtained by having at least one of said resonance peaks of at least two sections being overlapping or coinciding.

[0050] The combination of said plurality of sections can be considered as a combined reflector, having a combination reflection action. Said optical amplification action of said active section and said combination reflection action of said combined reflector are causing lasing at least one of the reflection wavelengths of said combined reflector.

[0051] Figure 6 shows an example of a possible configuration although the invention is not limited hereto. The active section (30) is optically at one side connected with a plurality of sections (120), said plurality of sections comprising a transmission filter (50) and three reflectors (90) (100) (110). The lasing light (10) leaves the laser at the other side of the active section. (20) indicates the amplification action within said active section (10). Said connections (40), (60), (70) and (80) indicate the optical interconnectivity and should not be considered as physical connections.

[0052] The transmission filters exploited in the invention have a transmission characteristic (150) with a plurality of transmission peaks. Alternatively it can be said that said transmission filters have spaced (spacing (130)) transmission maxima points providing a maximum transmission of an associated wavelength. The reflectors exploited in the invention have reflection characteristic (160) with a plurality of reflection peaks. Alternatively it can be said that said reflectors have spaced (spacing period (140)) reflective maxima points providing a maximum reflection of an associated wavelength. The spacing (130) (140) of said transmission or reflective maxima points of at least two of said sections are selected to be different. Said laser is therefore denoted an integrated semiconductor laser with different reflection or transmission sections. The transmission and reflection characteristic of said transmission filters and reflectors are positioned such that only one said transmission or reflective maxima of each of said sections being overlapping, meaning having a transmission or reflective maxima for the same frequency. Due to the different spacings of said transmission or reflective maxima points a small shift of one of said transmission or reflective maxima points results in an optical laser having a wide tunability. Said laser is therefore denoted widely wavelength tunable integrated semiconductor laser. Said shift can be due to current injections in said transmission or reflective sections. It can be said that said laser comprises of means for injecting current into part of said plurality of sections, resulting in said transmission or reflection characteristic being shifted in wave-

length.

[0053] The configuration of Figure 6 can for instance be achieved by using a power splitter (200) for connecting section (50) with sections (90) (100) (110). Said power splitter has a single port side (side connected to (50)) and a multi port side (side connected to (90)(100)(110)), with three ports.

[0054] A schematic view of a prior art GCSR laser structure is shown in Figure 2, showing an active section (600), a coupler section (610), a phase section (620), and a reflector (630), and the cross sections of said sections. Said coupler section and said reflector section have an essentially different resonance characteristic. Said coupler section does not have spaced resonance maxima points.

[0055] In a first embodiment a Y-structure as in Figure 3 is proposed with two reflectors (710), (720), placed on the same side of the active region (700). These two reflectors use sampled or super structure gratings to provide reflection combs with different periods; their design is the same as for (S)SG-DBR lasers. The power splitter (730) is used to split/combine the light leaving/entering the active region. Two phase control sections (740), (750) are shown in Figure 3. One provides the correct phase relation between the signals reflected by the two reflectors, whereas the second provides control of the overall phase of the combined reflected signal. According to an alternative embodiment, a separate phase control section could be placed in each of the arms of the Y. The branches of the Y-structure could be all-active, thus avoiding a (technologically more complex) transition from an active waveguide to a passive one. However, this has the disadvantage that the device will be more difficult to control, because power and wavelength control will be mixed. Therefore, passive waveguides for both branches of the Y-structure are preferred.

[0056] In a second embodiment a second structure, which in a top view looks like in Figure 8, is proposed. In this structure a plurality of reflectors (440) (including reflectors (410, 420, 430)) are placed on the same side of the active region. At least two of said reflectors use sampled or super structure gratings to provide reflections combs. At least two of said reflectors have reflection combs with different periods. The design of said reflectors is the same as for (S)SG-DBR lasers. The power splitter (450) is used to split and combine the light leaving/entering the active region. Phase control sections can be introduced. In one configuration one phase control section is placed between the active region and the reflectors and in all reflectors, except one, also a phase control section is provided. In another configuration only phase control sections are provided in said reflectors.

[0057] In a third embodiment a third structure, as shown in Figure 4, is proposed. The reflector consists of an active section (830), a ring resonator (800), which has a comb-shaped transmission characteristic (Figure 5) and a (S)SG-reflector (810) with potentially even an anti-reflective coating (820). The operation of a ring res-

onator is similar to that of a classic Fabry-Perot resonator, which can easily be understood if one thinks of the cross-coupling of the two couplers in the ring as being the transmission mirrors in the FP-resonator. The tuning is again based on the "Vernier"-principle, as in conventional (S)SG-DBR lasers: the ring resonator and the (S) SG-reflector are designed to have slightly different peak-spacing in their transmission and reflection characteristics respectively, and lasing occurs at or near the wavelength where two peaks overlap each other. A phase section, used to align a longitudinal cavity mode with the two aligned peaks, could also be included in this structure. It could be placed either between the active section and the ring resonator, or between the ring and the (S)SG-reflector.

[0058] In a fourth embodiment a fourth structure, as shown in Figure 9, is proposed. This structure comprises an active region (900) bounded at one side by a serial concatenation of sections, being a plurality of transmission filters (940), including filters (910)(920), said concatenation ends with a reflector (930). At least two of said sections, being either transmission filter or reflector, have a comb-shaped transmission characteristic. At least two of said sections, being either transmission filter or reflector, are designed to have a slightly different peak-spacing in their characteristic. A phase section can be placed between any of said sections and between said active section and said sections. Said transmission filters can be either (S)SG-transmission filters or a ring-resonator. Said reflector is a (S)SG-reflector.

[0059] A main feature of the proposed Y and ring-structures and any structure, exploiting a combination of the principles on which the proposed Y and ring structures are based, is that light is emitted directly from the active region without going through a passive region. This is expected to result in a higher efficiency and a lower degree of power variation during tuning. Typical reflectors can be designed to have a uniform envelope of the reflection peaks. These designs require long passive waveguides and the reflectivity at the reflection peaks is quite high. Both of these factors lead to a reduced efficiency in a two-sided reflector structure. In all proposed structures the output power is not passing through a reflector, hence a high efficiency can be expected, and the high reflectivity is now an advantage. Therefore in the invention all said sections are optically connected to one side of said active region.

[0060] Since the reflectors are preferably passive, the Y structure (of the first embodiment) and the structure of the second embodiment, does not suffer from the control problems present in the Y-laser, known from prior art.

[0061] The performance with respect to tuning and output power is expected to be similar to that of a GCSR laser, but the fabrication is easier. The number of process steps will be the same as for an SG/SSG, but lower than for a GCSR laser. Except for mask design the fabrication is nearly identical to that for SG/SSG DBR la-

sers, but AR coating of the facets may not be necessary when the grating is designed for high peak reflectivity. As an alternative one could use an absorbing region to kill off any unwanted reflection from the facet.

- 5 [0062] There may be some radiation losses associated with the power splitter in the Y-laser, but these are unlikely to be higher than the radiation losses in the tunable coupler section of the GCSR.

10

Claims

- 15 1. An apparatus comprising a substrate made of a semiconducting material, a plurality of sections on said substrate (120), all said sections being connected together, at least two of said sections being resonators, each including a waveguide system and having spaced resonance maxima points providing a maximum resonance with an associated wavelength, wherein the spacing of at least two of said resonance maxima points of the respective sections being essentially not equal, and at least one of said resonance maxima of each of two said sections being resonators overlapping each other.
- 25 2. The apparatus as recited in claim 1, wherein only one of said resonance maxima of each of said sections being resonators overlapping each other.
- 30 3. The apparatus as recited in claim 1 or 2, wherein said resonator is either a transmission filter (50), having spaced transmission maxima points (130) providing a maximum transmission with an associated wavelength as resonance maxima points or a reflector (90), (100), (110), having spaced reflective maxima points (140) providing a maximum reflection with an associated wavelength as resonance maxima points.
- 40 4. The apparatus according to anyone of the preceding claims further comprising a two-sided active radiation-generating section (30) on said substrate, said plurality of sections being connected to one side of said two-sided active section.
- 45 5. The apparatus according to anyone of the preceding claims, wherein at least one of said plurality of sections is inactive.
- 50 6. The apparatus according to anyone of the preceding claims, wherein at least one of said plurality of sections is active.
- 55 7. The apparatus according to anyone of the preceding claims, wherein at least one of said waveguide systems has a periodically broken short-period structure including short period stripped regions alternating with non-stripped regions.

8. The apparatus according to anyone of the preceding claims 1 to 7, wherein at least one of said waveguide systems has a diffractive grating having a plurality of repeating unit regions each having a constant length, thus forming a modulation period, and at least one parameter that determines the optical reflectivity or transmission of said diffractive grating varying depending on its position in each of said repeating unit regions along a direction of optical transmission in said laser, said diffractive grating extending by at least two modulation periods. 5
9. The apparatus according to anyone of the preceding claims 1 to 7, wherein at least one of said waveguide systems is a ring resonator (800). 10
10. The apparatus according to anyone of the preceding claims 6 to 9, wherein said active section is creating a light beam by spontaneous emission over a bandwidth around one center frequency and guiding said light beam and having optical amplification actions. 15
11. The apparatus as recited in claim 10, wherein the combination of said plurality of sections has a combined reflection action and said optical amplification action of said active section causing lasing at at least one of the reflection wavelengths of said combination. 20
12. The apparatus according to anyone of the preceding claims 6 to 11, further comprising a plurality of power splitters (200), being used for connecting some of said plurality of sections and connecting to said active section. 25
13. The apparatus as recited in claim 6 to 12, wherein said apparatus is a serial concatenation of said active section (900) and a plurality of said sections (910), (920), (930). 30
14. The apparatus as recited in claim 12, wherein a connection of said active section (400) is performed to one single port side of a power splitter (450) with a parallel connection of a plurality of sections (410), (420), (430) to the other multi port side of said power splitter. 35
15. The apparatus according to anyone of the preceding claims, further comprising a plurality of phase sections, being used for adjusting the round trip cavity phase. 40
16. The apparatus according to anyone of the preceding claims, further comprising means for injecting current into at least some of said sections being a resonator in order to have said transmission or reflection characteristic being shifted in wavelength. 45
17. A method for setting lasing frequencies of an apparatus, comprising a substrate made of semiconducting material, a plurality of connected sections on said substrate, with at least two of said sections, being resonators having spaced resonance maxima points providing a maximum resonance with an associated wavelength, wherein the spacing of at least two of said resonance maxima points of the respective sections being essentially not equal, said method comprising the step of) positioning said resonance maxima points of said resonators such that a plurality of said resonance maxima of each of said sections being resonators overlapping each other, said plurality defining said lasing frequencies. 50
18. A method for changing the lasing frequency of an apparatus as recited in claim 1 from a first frequency to a second frequency, said second frequency being spaced from said first frequency by a first distance, said apparatus, comprising a substrate made of semiconducting material, a plurality of connected sections on said substrate, with at least two of said sections, being resonators, having spaced resonance maxima points providing a maximum resonance with an associated wavelength, wherein the spacing of at least two of said resonance maxima points of the respective sections being essentially not equal, said method comprising the step of changing the relative position of said resonance maxima points of said resonators with a second distance, being substantially smaller than said first distance. 55
19. The use of the apparatus as recited in claim 4 as an integrated/semiconductor tunable optical laser.

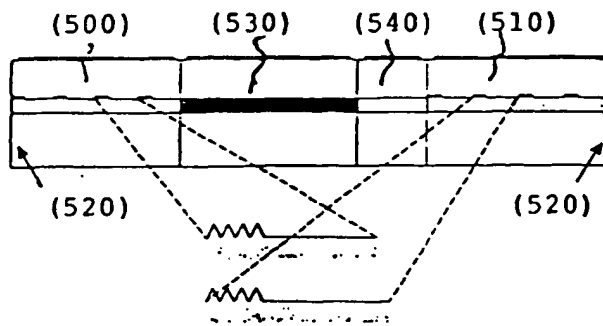


FIG. 1

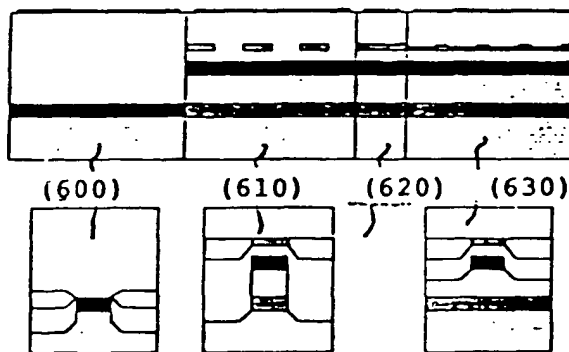


FIG. 2

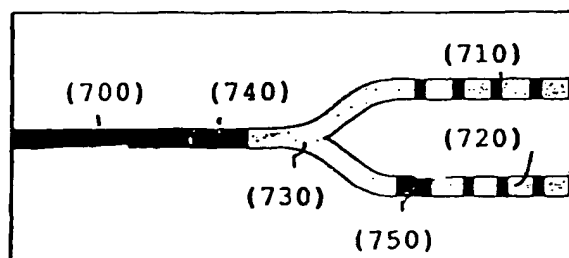


FIG. 3

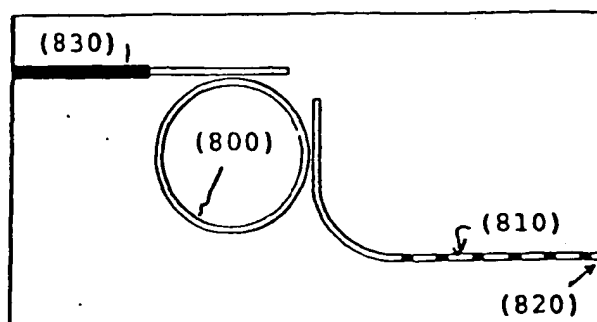


FIG. 4

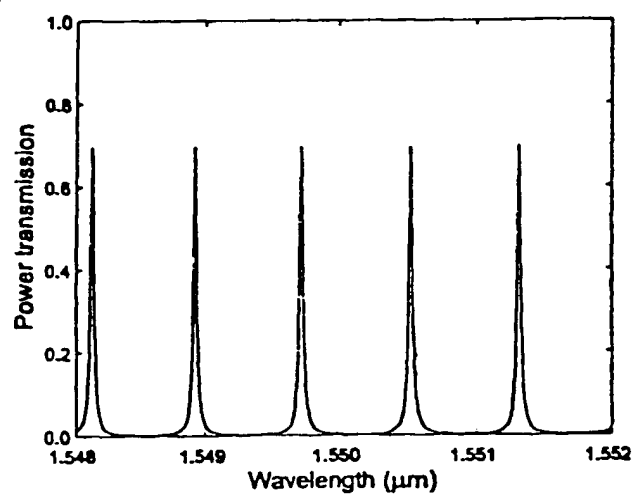


FIG. 5

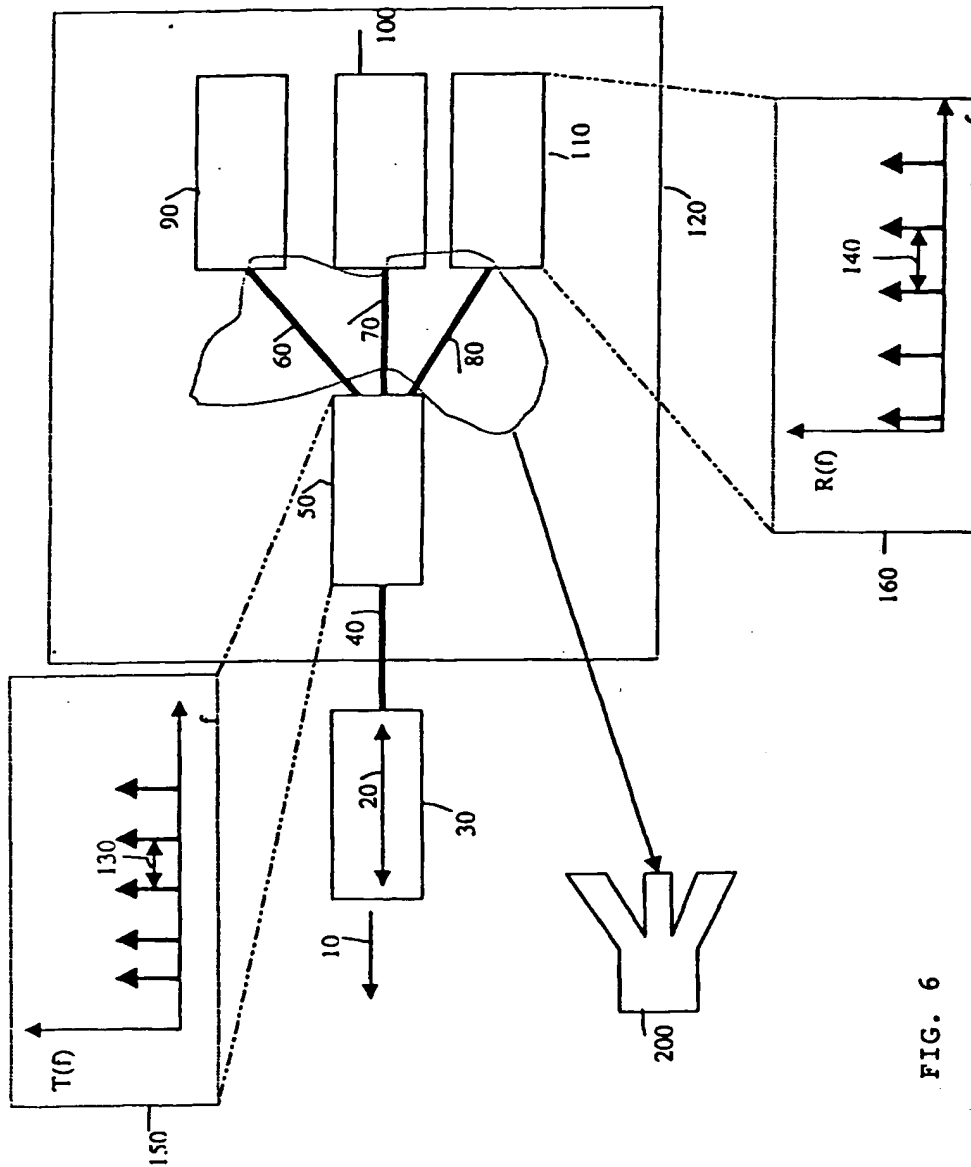


FIG. 6

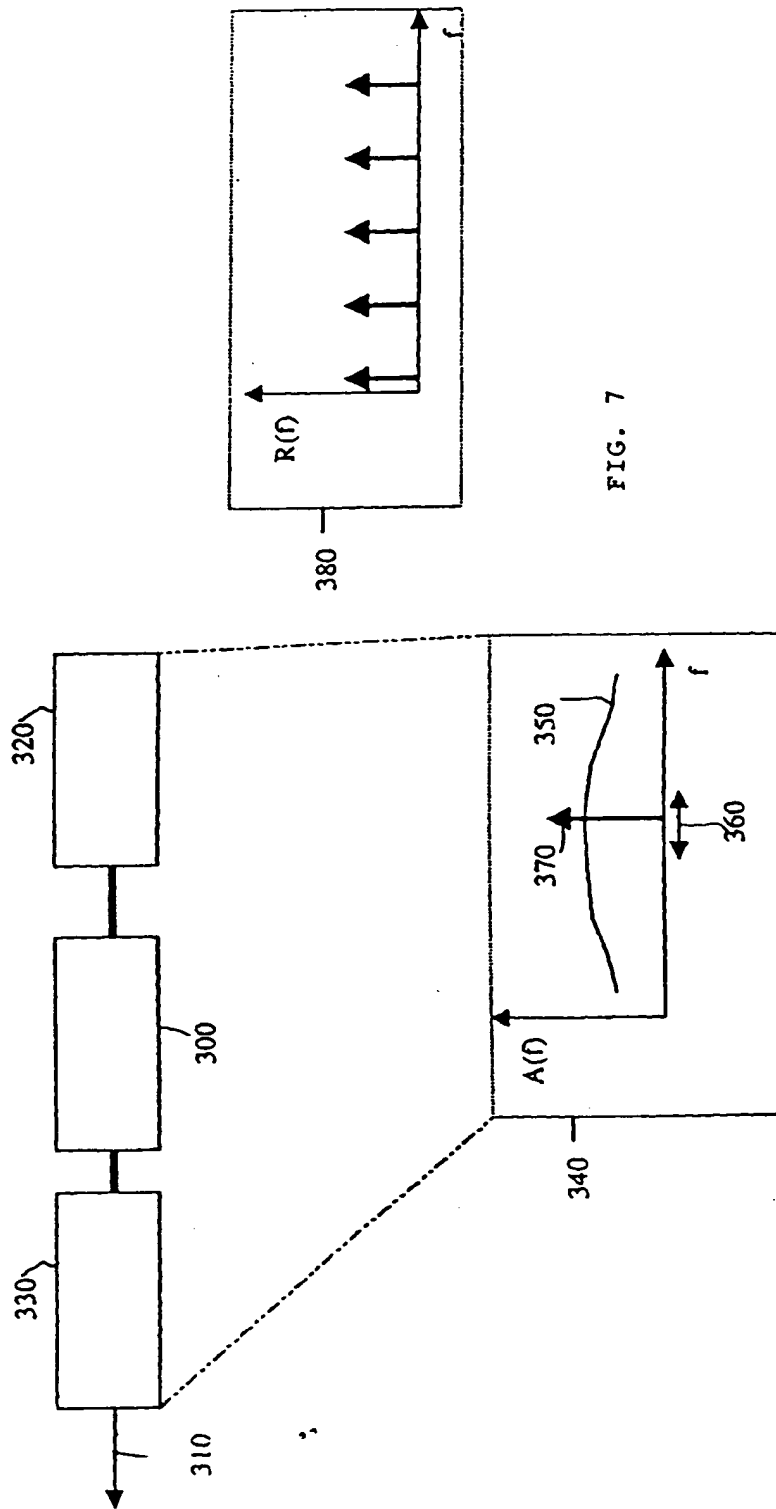


FIG. 7

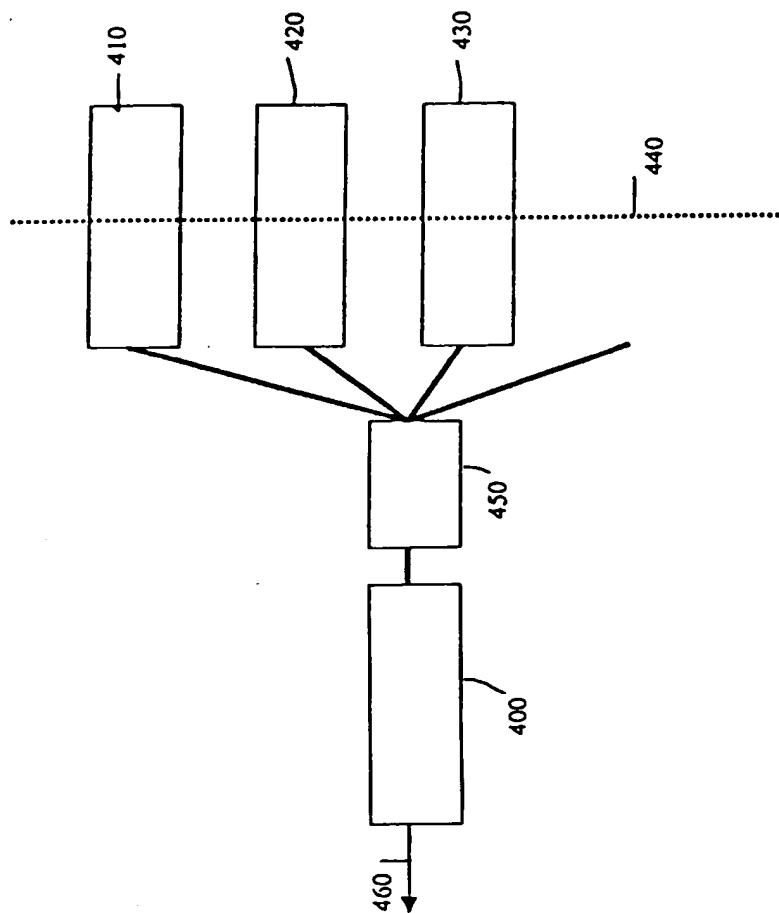


FIG. 8

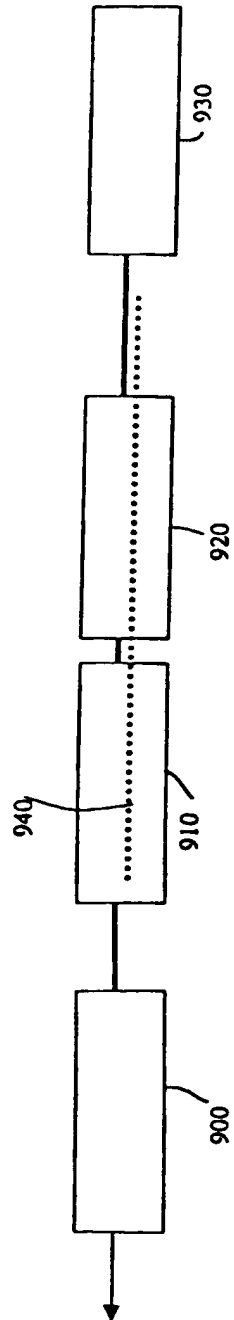


FIG. 9



European Patent
Office

EUROPEAN SEARCH REPORT

Application Number
EP 99 87 0214

DOCUMENTS CONSIDERED TO BE RELEVANT			
Category	Citation of document with indication, where appropriate, of relevant passages	Relevant to claim	CLASSIFICATION OF THE APPLICATION (Int.Cl.7)
X	WOLF T ET AL: "LASER DIODES AND INTEGRATED OPTOELECTRONIC CIRCUITS FOR FIBER OPTICAL APPLICATIONS" EUROPEAN TRANSACTIONS ON TELECOMMUNICATIONS AND RELATED TECHNOLOGIES, IT, AEI, MILANO, vol. 4, no. 6, 1 November 1993 (1993-11-01), pages 599-614, XP000433717 ISSN: 1120-3862	1-6, 10-12, 14, 16-19	H01S5/026 H01S5/12 H01S5/0625
Y	* page 607, paragraph 3.2; figure 10 *	1,5-8	
Y	PATENT ABSTRACTS OF JAPAN vol. 013, no. 026 (E-706), 20 January 1989 (1989-01-20) & JP 63 229796 A (FUJITSU LTD), 26 September 1988 (1988-09-26) * abstract *	1,5-8	
X	EP 0 926 787 A (NORTHERN TELECOM LTD) 30 June 1999 (1999-06-30) * column 3, line 53 - column 4, line 8 * * column 9, line 1-11 * * column 10, line 10-42; figures 4-7 *	7,8,13, 17	TECHNICAL FIELDS SEARCHED (Int.Cl.7) H01S
A	US 5 651 018 A (LANG ROBERT J ET AL) 22 July 1997 (1997-07-22) * figures 24,25 *	1-19	
A	TALNEAU A ET AL: "CONSTANT OUTPUT POWER AND LOW LINEWIDTH IN A SIMPLE WIDE-TUNING DFB LASER WITH MULTIWAVELENGTH GRATING" IEEE JOURNAL OF SELECTED TOPICS IN QUANTUM ELECTRONICS, US, IEEE SERVICE CENTER, vol. 3, no. 2, 1 April 1997 (1997-04-01), pages 628-631, XP000735963 ISSN: 1077-260X * figures 1,2 *	1,7,13, 17	
The present search report has been drawn up for all claims			
Place of search THE HAGUE		Date of completion of the search 23 March 2000	Examiner Claessen, L
CATEGORY OF CITED DOCUMENTS X : particularly relevant if taken alone Y : particularly relevant if combined with another document of the same category A : technological background O : non-written disclosure P : intermediate document		T : theory or principle underlying the invention E : earlier patent document, but published on, or after the filing date D : document cited in the application L : document cited for other reasons & : member of the same patent family, corresponding document	

EPO FORM 1503 03.02 (PatCo1)



European Patent
Office

EUROPEAN SEARCH REPORT

Application Number
EP 99 87 0214

DOCUMENTS CONSIDERED TO BE RELEVANT			
Category	Citation of document with indication, where appropriate, of relevant passages	Relevant to claim	CLASSIFICATION OF THE APPLICATION (Int.Cl.7)
D,A	US 5 325 392 A (TAMAMURA TOSHIAKI ET AL) 28 June 1994 (1994-06-28) * the whole document *	1-19	
D,A	KUYNETSOV M: "DESIGN OF WIDELY TUNABLE SEMICONDUCTOR THREE-BRANCH LASERS" JOURNAL OF LIGHTWAVE TECHNOLOGY, US, IEEE, NEW YORK, vol. 12, no. 12, 1 December 1994 (1994-12-01), pages 2100-2106, XP000493715 ISSN: 0733-8724 * the whole document *	1-19	
A	US 5 398 256 A (HOHIMER JOHN P ET AL) 14 March 1995 (1995-03-14) * the whole document *	1,9	
The present search report has been drawn up for all claims			TECHNICAL FIELDS SEARCHED (Int.Cl.7)
Place of search THE HAGUE		Date of completion of the search 23 March 2000	Examiner Claessen, L
<p>CATEGORY OF CITED DOCUMENTS</p> <p>X : particularly relevant if taken alone Y : particularly relevant if combined with another document of the same category A : technological background O : non-written disclosure P : intermediate document</p> <p>T : theory or principle underlying the invention E : earlier patent document, but published on, or after the filing date D : document cited in the application L : document cited for other reasons</p> <p>Δ : member of the same patent family, corresponding document</p>			

EPO FORM 1503 (03/02) (P/A/C31)

ANNEX TO THE EUROPEAN SEARCH REPORT
ON EUROPEAN PATENT APPLICATION NO.

EP 99 87 0214

This annex lists the patent family members relating to the patent documents cited in the above-mentioned European search report. The members are as contained in the European Patent Office EDP file on
The European Patent Office is in no way liable for these particulars which are merely given for the purpose of information.

23-03-2000

Patent document cited in search report	Publication date	Patent family member(s)	Publication date
JP 63229796 A	26-09-1988	NONE	
EP 0926787 A	30-06-1999	JP 11251691 A	17-09-1999
US 5651018 A	22-07-1997	US 5537432 A	16-07-1996
		US 5392308 A	21-02-1995
		US 5914978 A	22-06-1999
		US 5592503 A	07-01-1997
		US 5499261 A	12-03-1996
		US 5602864 A	11-02-1997
		US 5864574 A	26-01-1999
		US 5696779 A	09-12-1997
		US 5703897 A	30-12-1997
		US 5894492 A	13-04-1999
US 5325392 A	28-06-1994	JP 2690840 B	17-12-1997
		JP 6061572 A	04-03-1994
		JP 2770897 B	02-07-1998
		JP 6061577 A	04-03-1994
		JP 2770900 B	02-07-1998
		JP 6069586 A	11-03-1994
		JP 2832920 B	09-12-1998
		JP 6053616 A	25-02-1994
		DE 69325118 D	08-07-1999
		EP 0559192 A	08-09-1993
		EP 0847116 A	10-06-1994
US 5398256 A	14-03-1995	NONE	

EPO FORM P0159

For more details about this annex : see Official Journal of the European Patent Office, No. 12/82